

# Calibration of the Reflection Grating Spectrometers

- Physical model
- Scientific performance
- Current SAS implementation
- Conclusions

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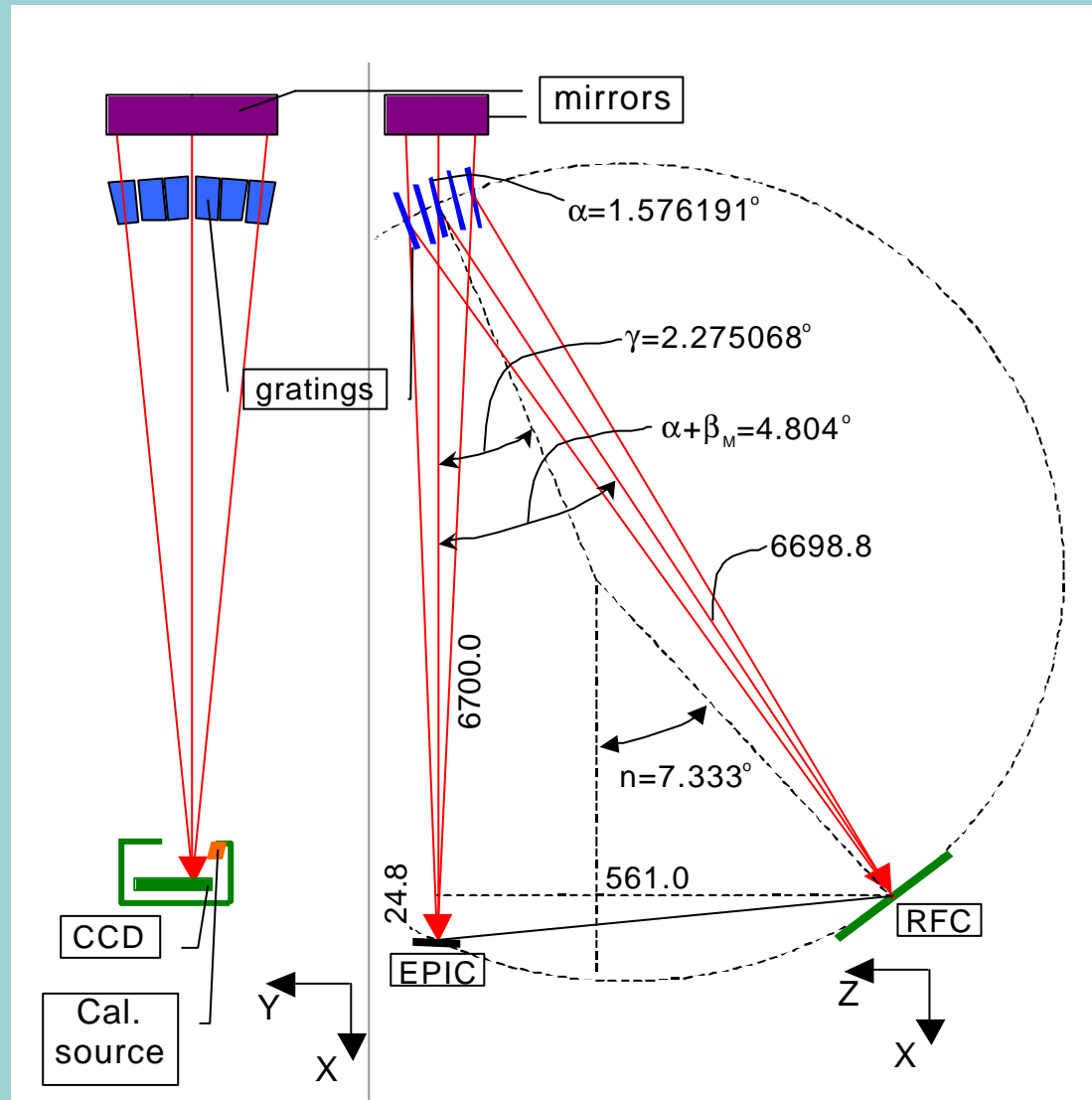


# Physical model

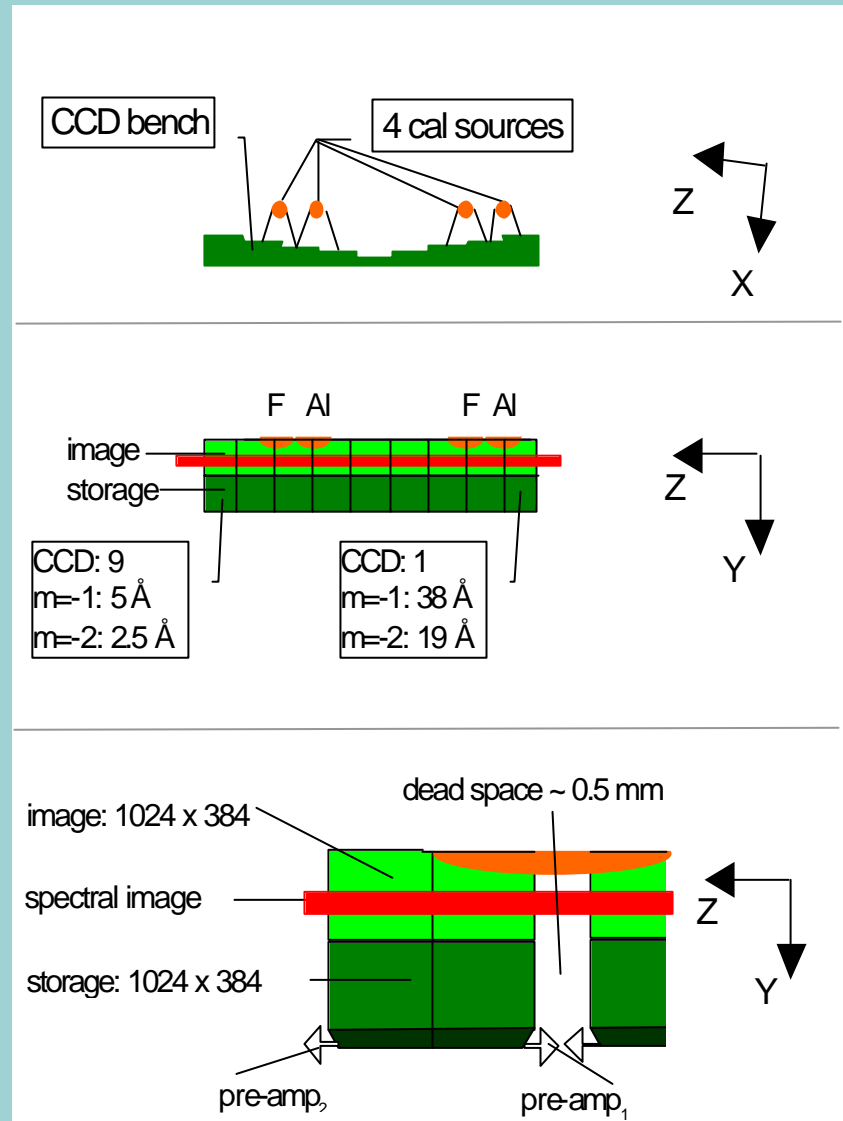
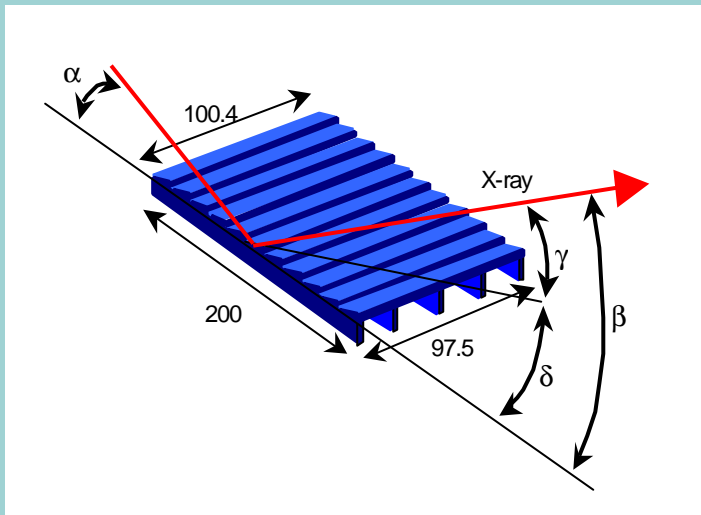
- Optical design
- Mirror response
- Grating response
- Camera/CCD response



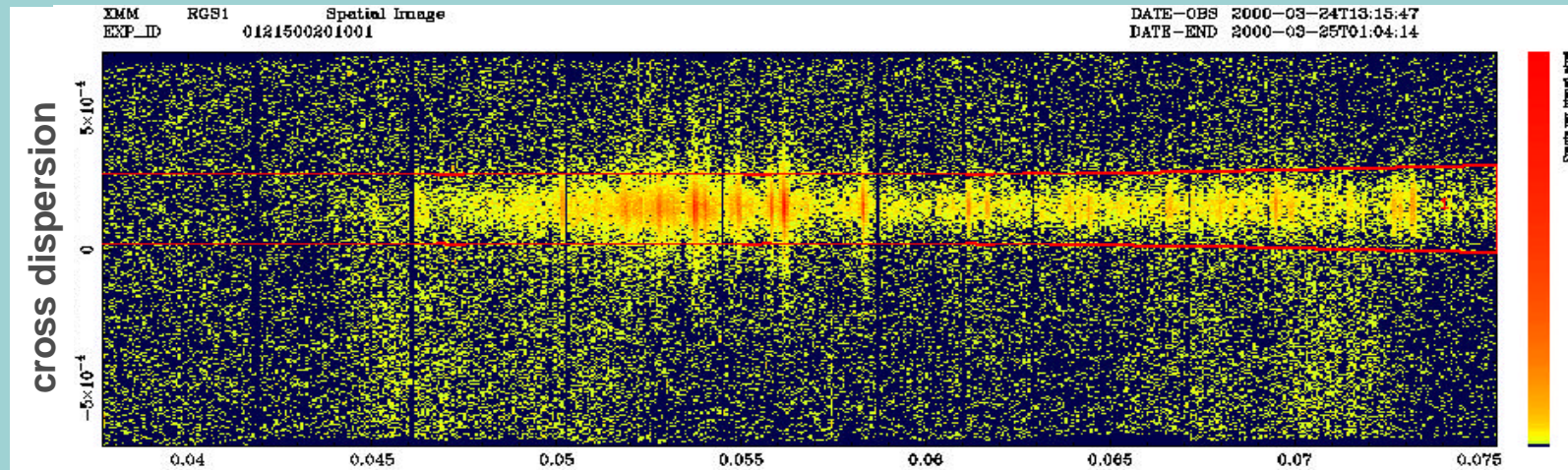
# Optical design (1)



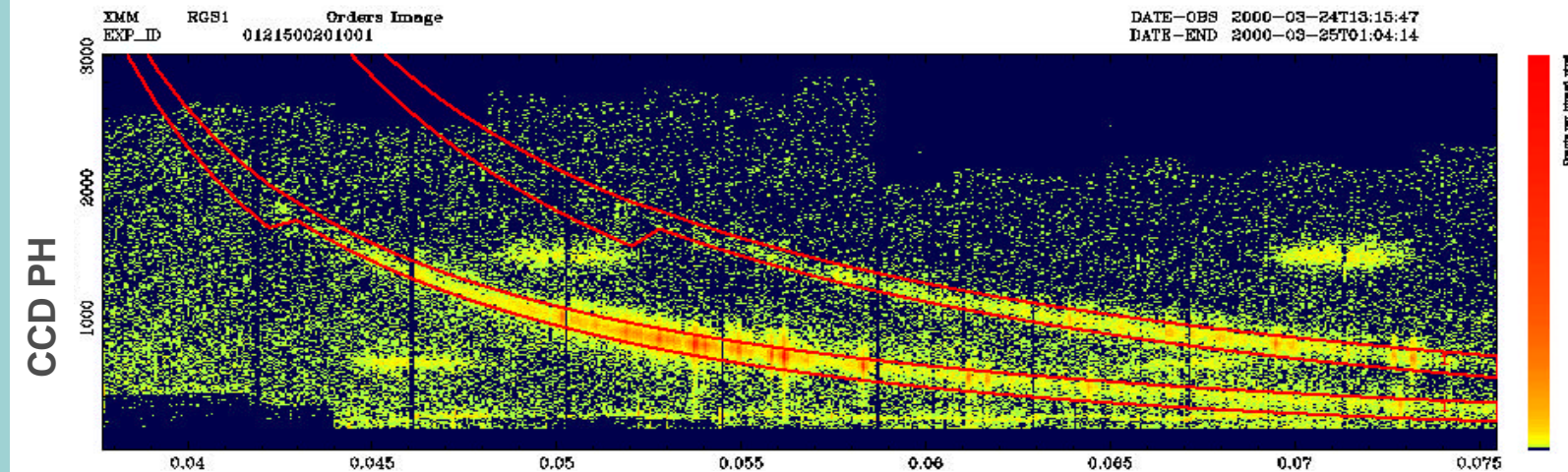
# Optical design (2)



# Optical design (3)



b, outgoing angle from gratings

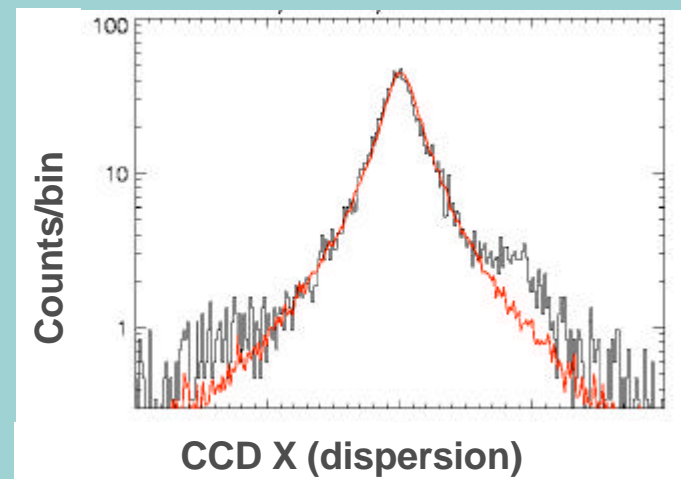
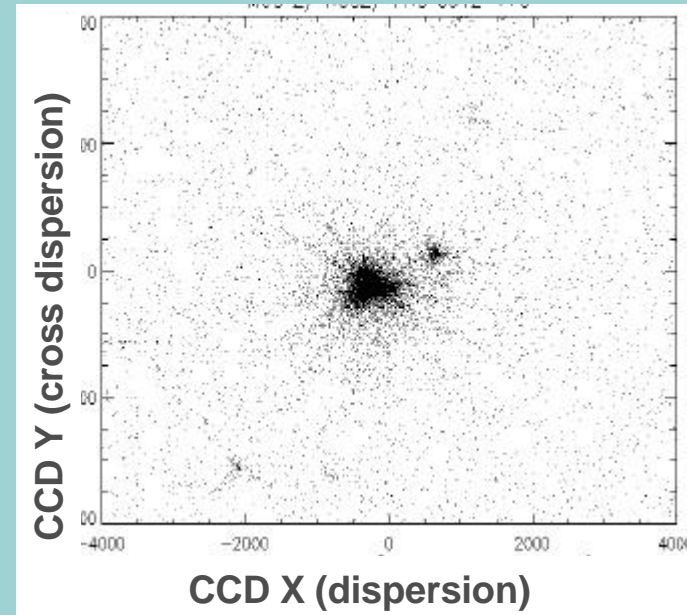


b, outgoing angle from gratings



# Mirror response

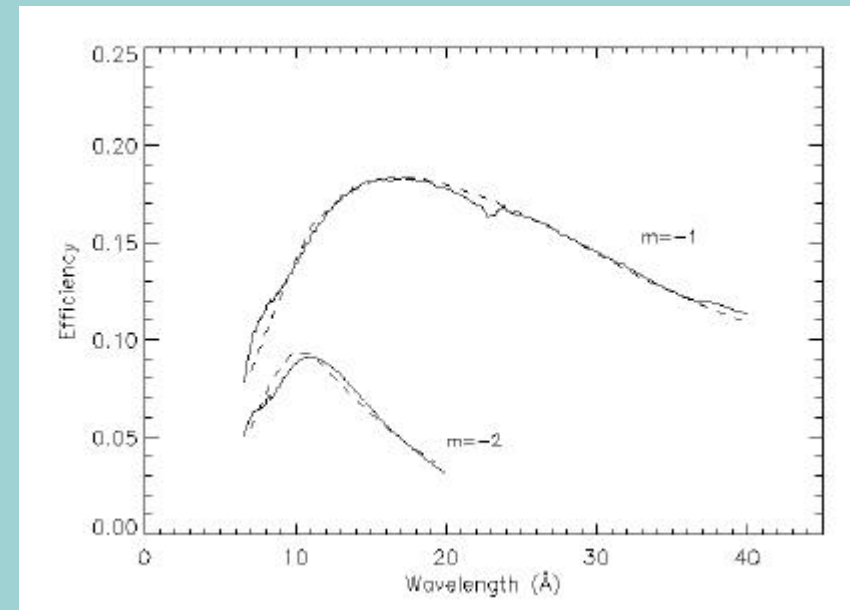
- Empirical fit to raytrace results (consistent with to flight data PKS 0312-770), projected on dispersion axis
- mirror effective area
- empirical fit to cross dispersion data (Mkr 421) on RGS detector (Rowland circle is not optical mirror focus)



# Grating response

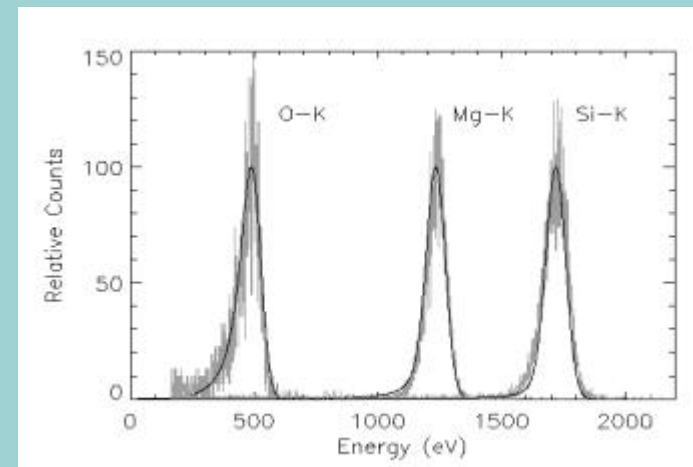
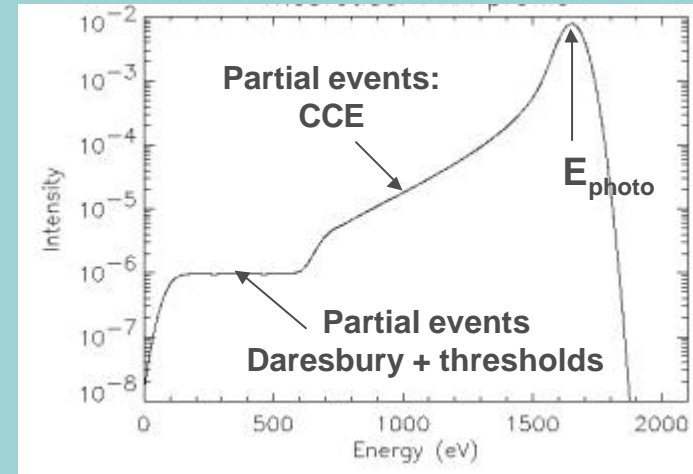
- Calculation of efficiency using Maxwell equations
- Fit blaze angle to various datasets (Bessy,  $\alpha$  dependence, orders)
- incoherent scattering (scalar theory) with two distributions (small and large angle) in the dispersion direction
- large angle scattering in cross dispersion direction
- Add alignment information

Bessy data and model



# CCD response: redistribution

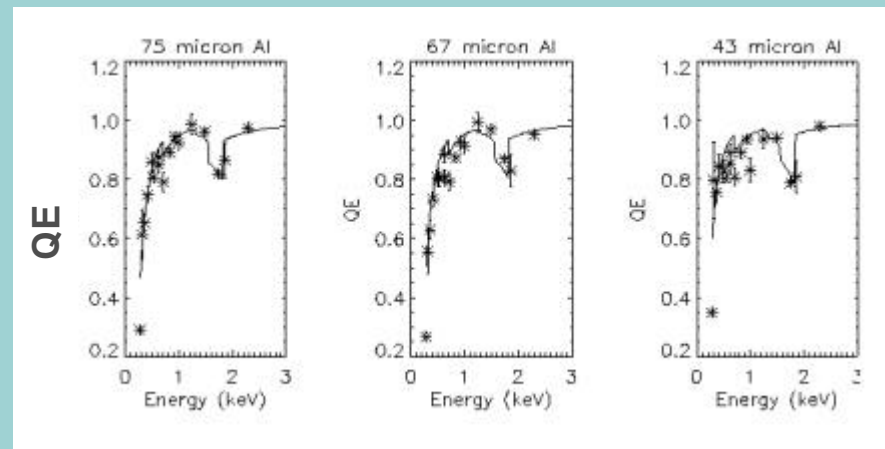
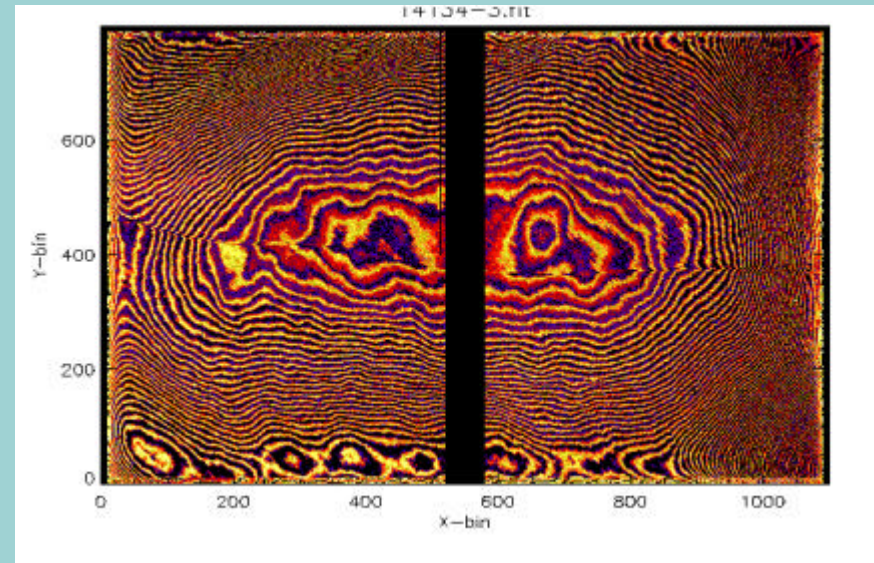
- CCD energy response used to separate orders (less critical)
- CCD redistribution function includes partial event tail and CCE at the backside
- CCD redistribution function verified in orbit as for a given position on the detector the energy is 'monochromatic'





# CCD response: QE

- QE based on CCD thickness (verified by IR) and thickness of various layers (optical Al filter of 45, 68 and 75 nm and MgF<sub>2</sub> insulation layer)
- QE verified during ground calibrations
- CTI/gain corrections determined in orbit using onboard calibrations sources (Al and F) as well as astrophysical objects



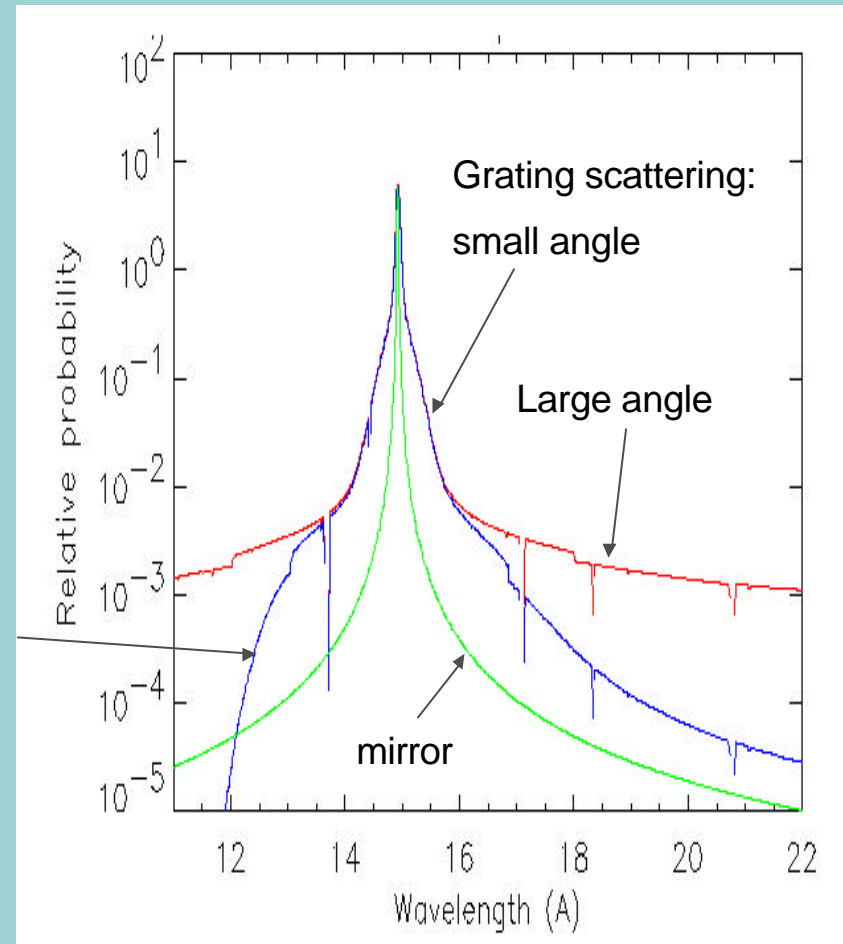
# Scientific performance

- Line spread function(LSF)
- Wavelength scale
- Effective area
- Background
- In-orbit monitoring



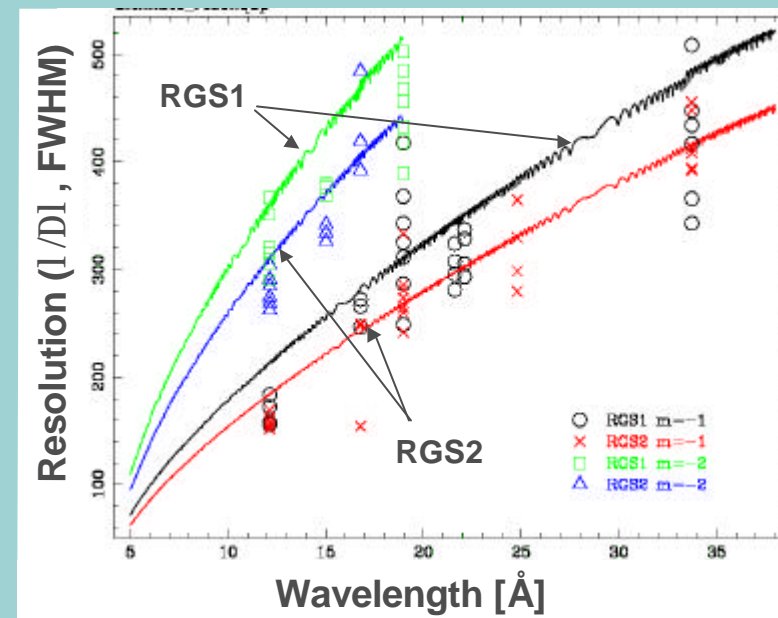
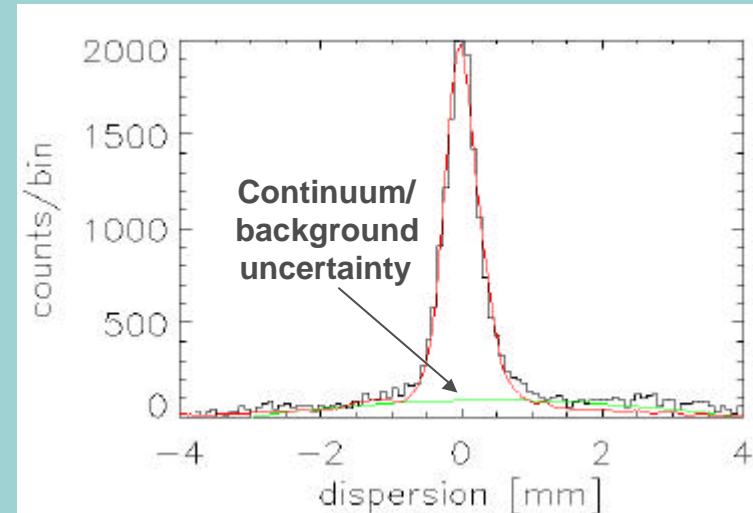
# Line spread function

- Expected LSF is convolution of
  - mirror response
  - grating response
  - and CCD response
  - (+ electronics)



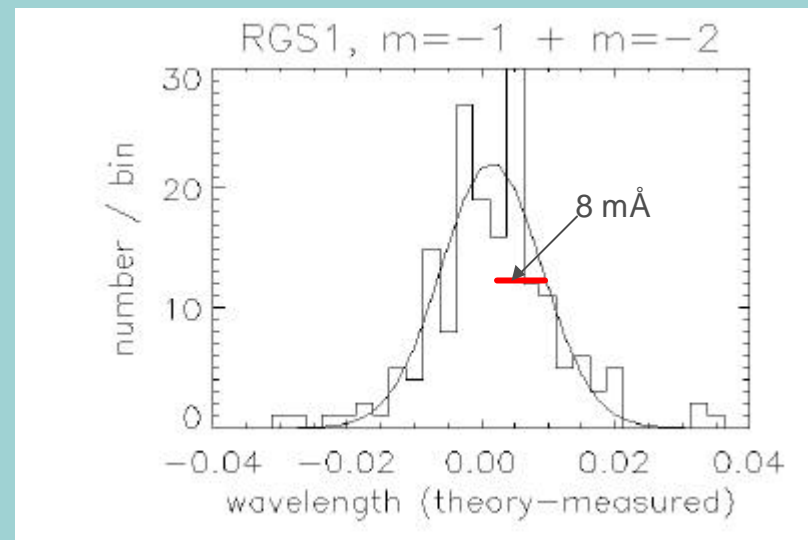
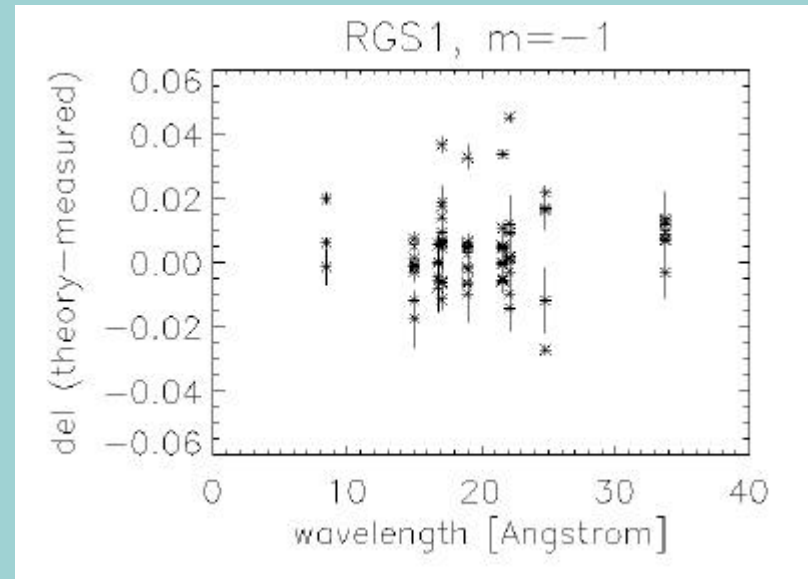
# In-orbit verification of the LSF

- Verified on number of strong unblended lines
- Model (raytrace) in good agreement with data (some uncertainty in background/continuum)
- Calculated response (FWHM) in good agreement with larger set of data



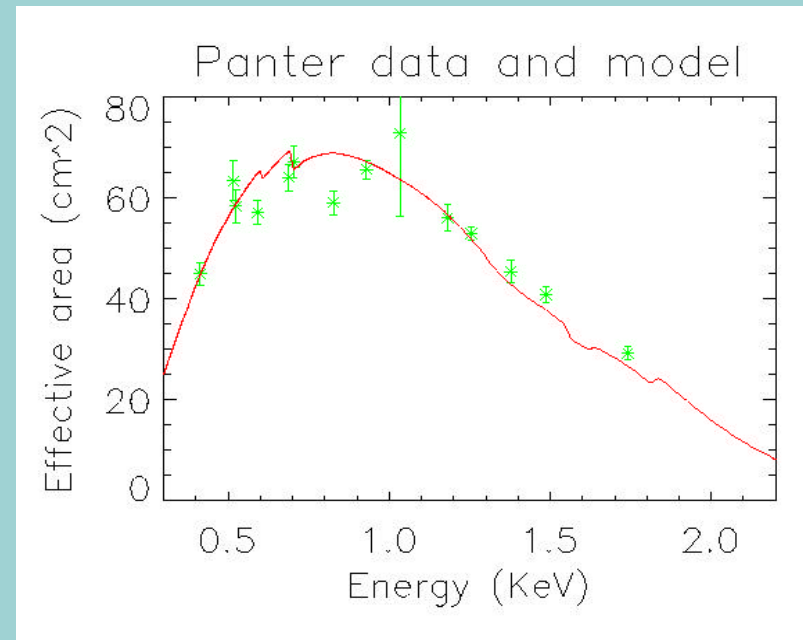
# 1 scale verification

- Ground alignment does not give ultimate accuracy
- Comparison of strong lines ( $\text{Ly}\alpha$ ) with laboratory wavelengths for a number of pointings
- Result:  $\pm 8\text{m}\text{\AA}$  ( $1\sigma$ )
- RGS1  $+ 1.5\text{ m}\text{\AA}$
- RGS2  $- 1.6\text{ m}\text{\AA}$



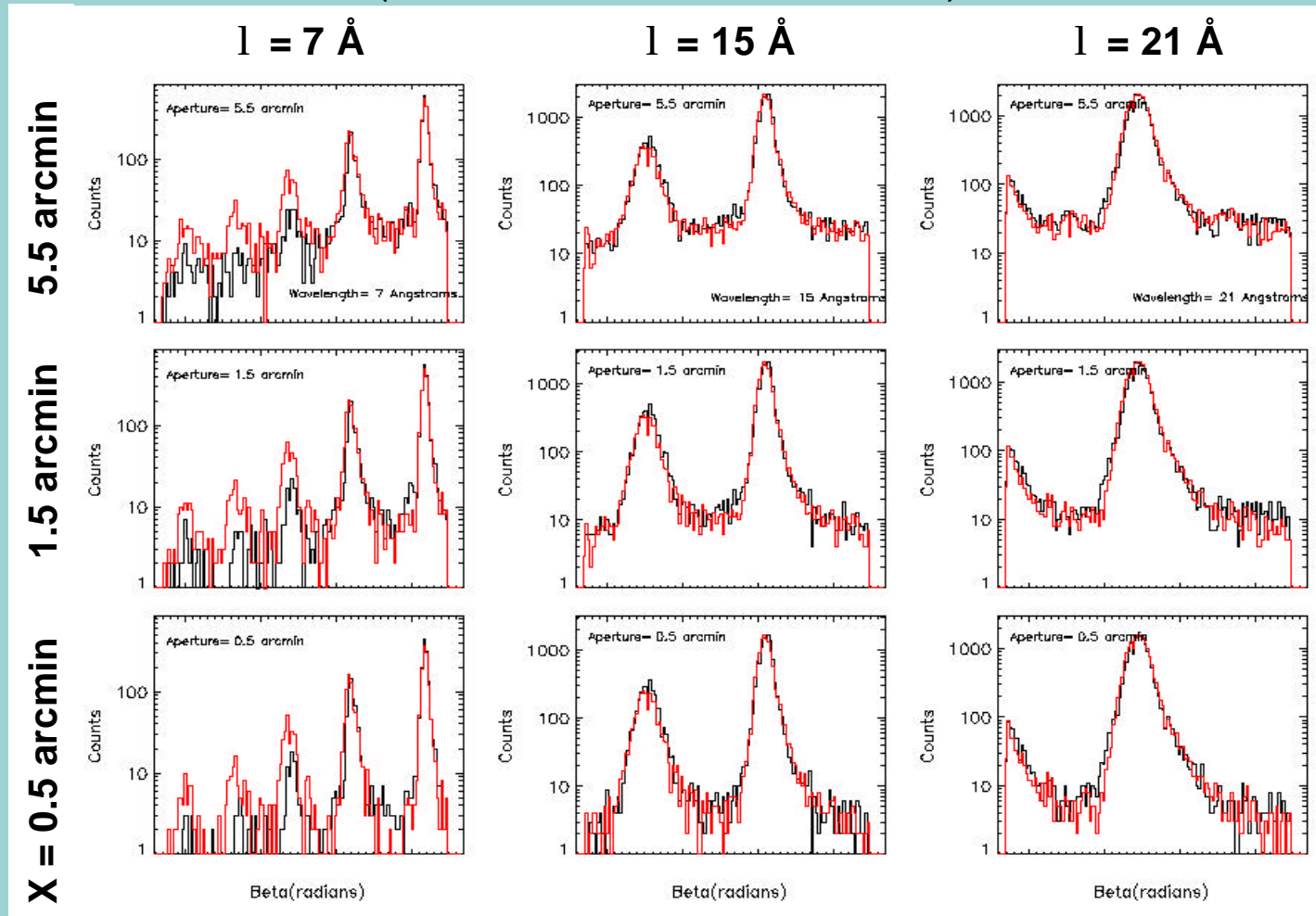
# Effective area

- Based on physical model
- Validated during long beam tests (which is not fully representative)
- Verified in-orbit on BL Lac (PKS2155) resulting in number of changes



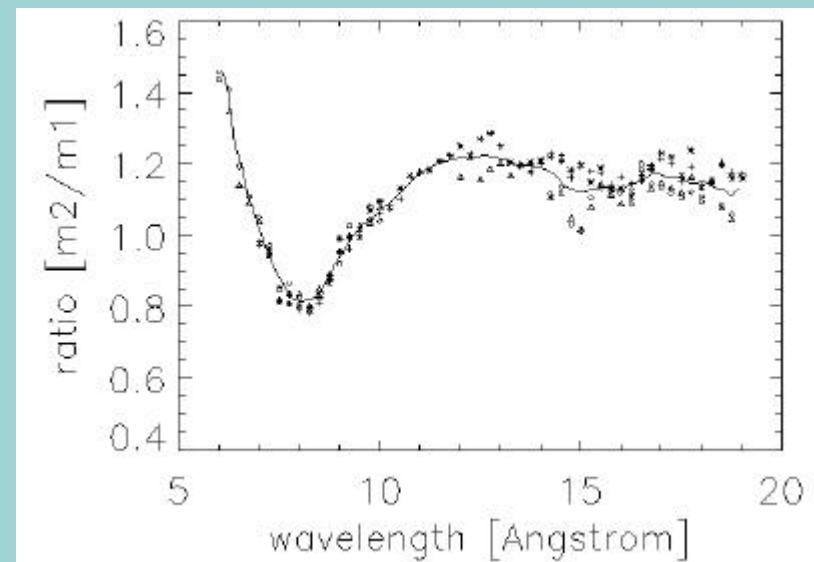
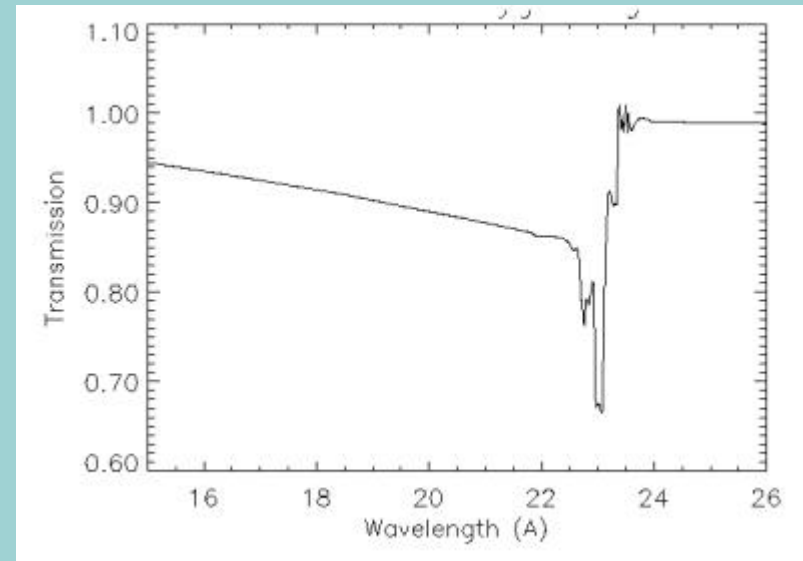
# Effective area 2

Optimization of scatter parameters to describe the flight data  
(red = model, black = data)



# Effective area (3)

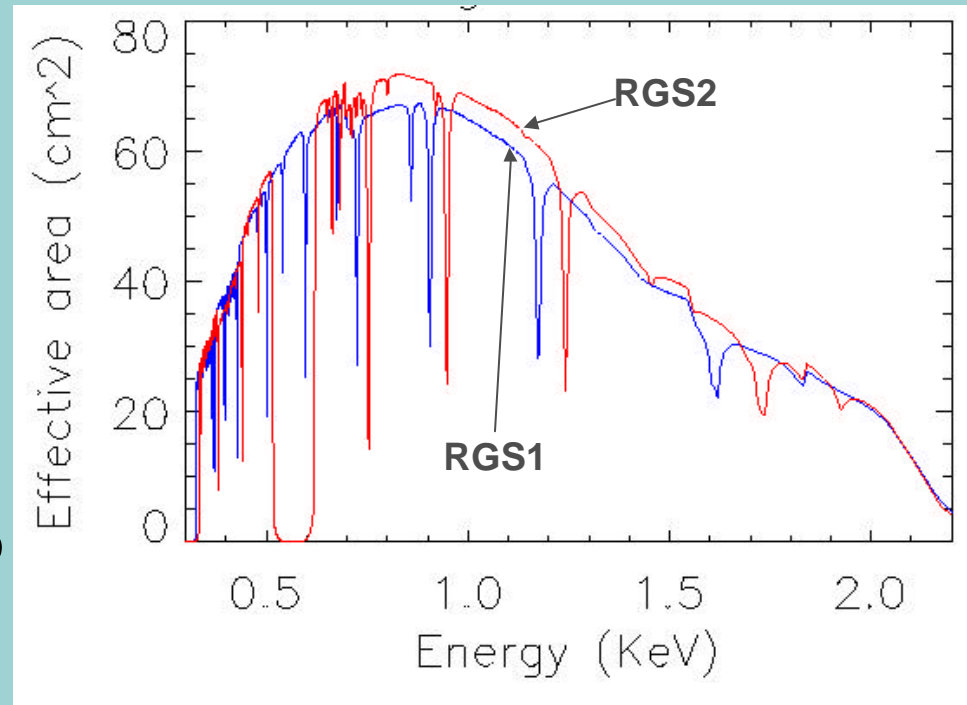
- Apply correction factors for:
  - Difference RGS1 and RGS2 (b dependent)
  - O-edge
  - Second order spectra





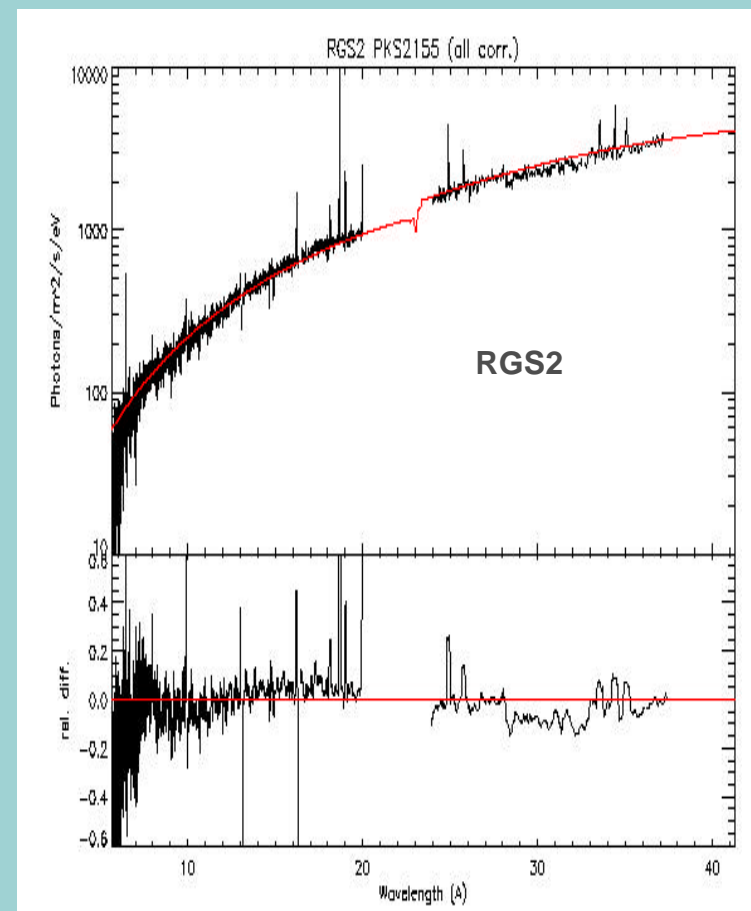
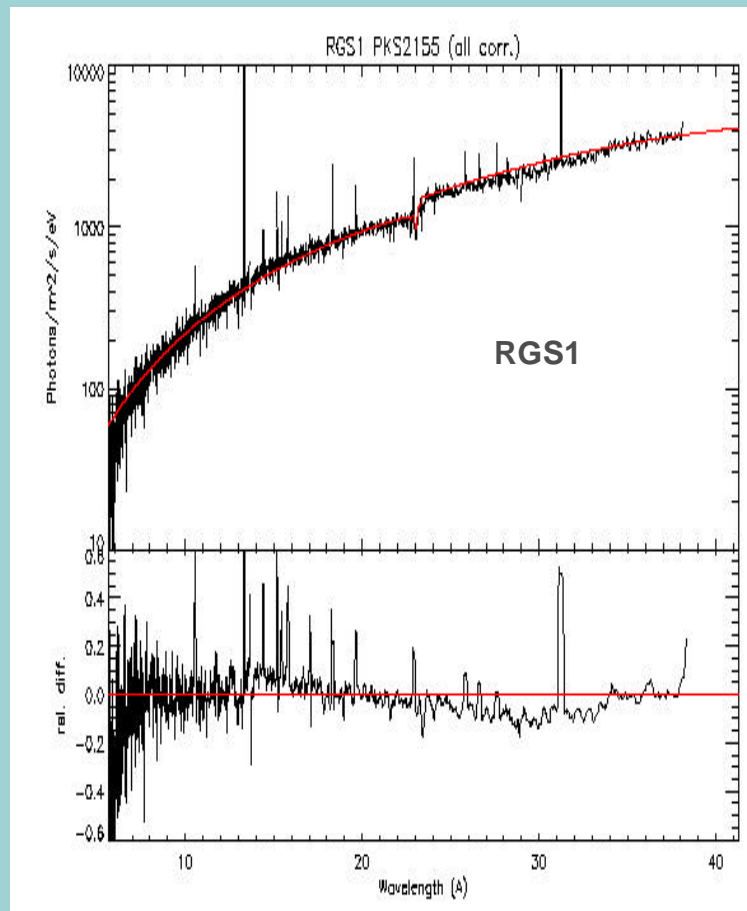
# Effective area: result

- Predicted effective area for RGS1 and RGS2
- includes hot columns and failing CCD chain (only shown for RGS2)
- No sharp features due to scattering wings
- Edges due to O, F, Mg and Al + finite thickness of Si ( $\sim 30 \mu\text{m}$ )



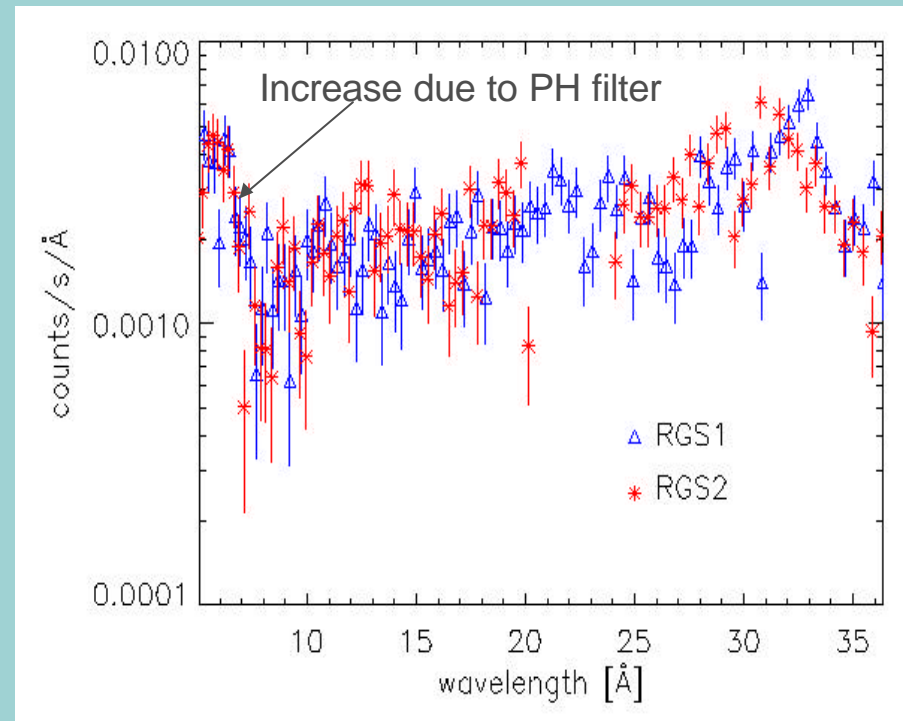
# Effective area: verification

- Result for PKS2155 consistent with single power law for both instruments (within 5% except for  $< 7 \text{ \AA}$ )



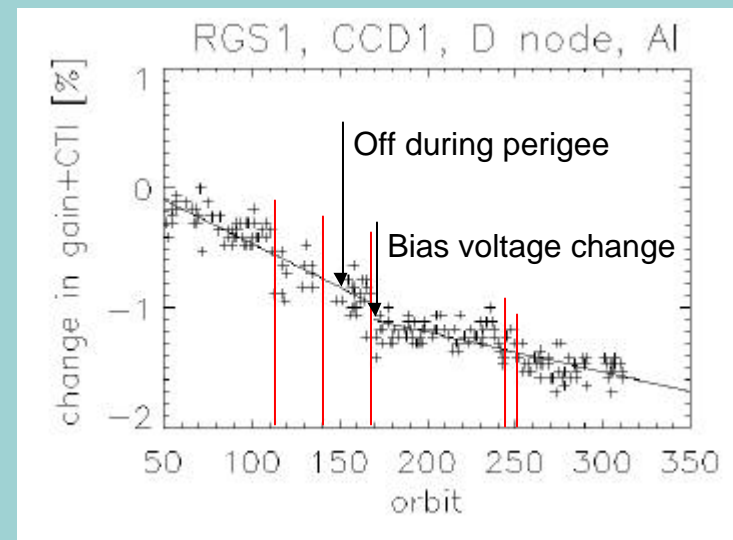
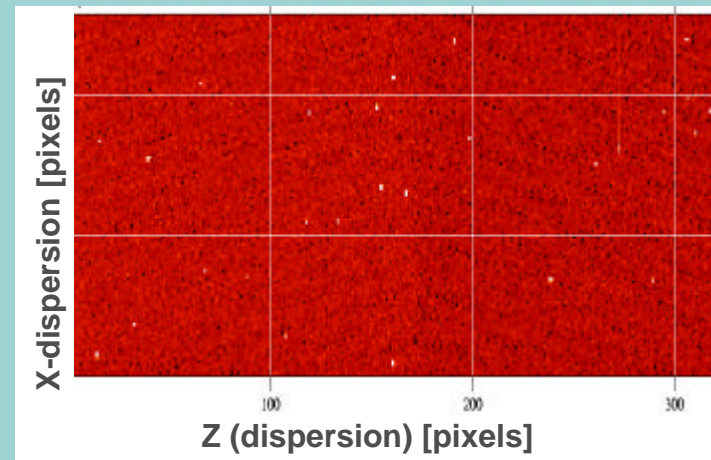
# Background

- Different background components:
  - Minimum ionizing particles
  - Electrons
  - Onboard calibration source
  - Fluorescence lines
  - Read-out noise
  - Soft protons entering the telescope (highly variable)



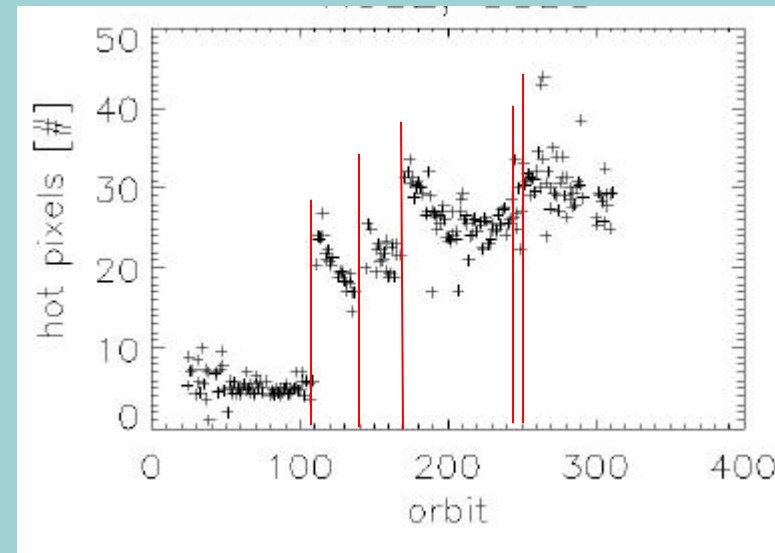
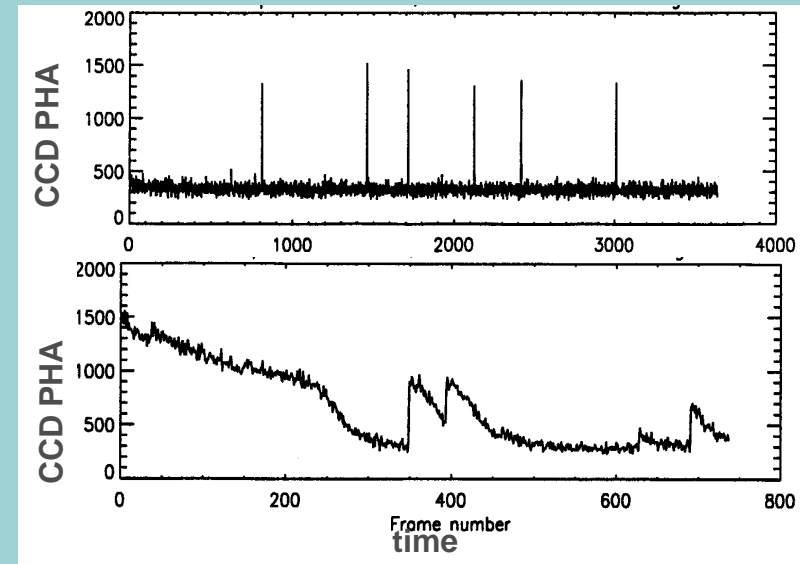
# In orbit monitoring (1)

- Dark current and optical load (
  - uniform, less than  $1 e^-$  contribution to read-out noise of  $5 e^-$ ,
  - few defects
  - Particle background
- CTI + gain (on chip amplifier and electronics)
  - Effect less than 1% (normalized on orbit 165)
  - Slope change, presumably since electronics is off during perigee



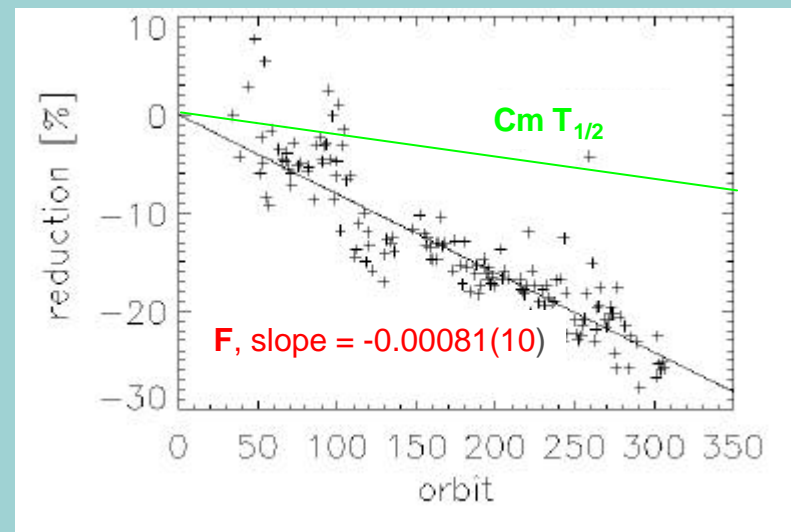
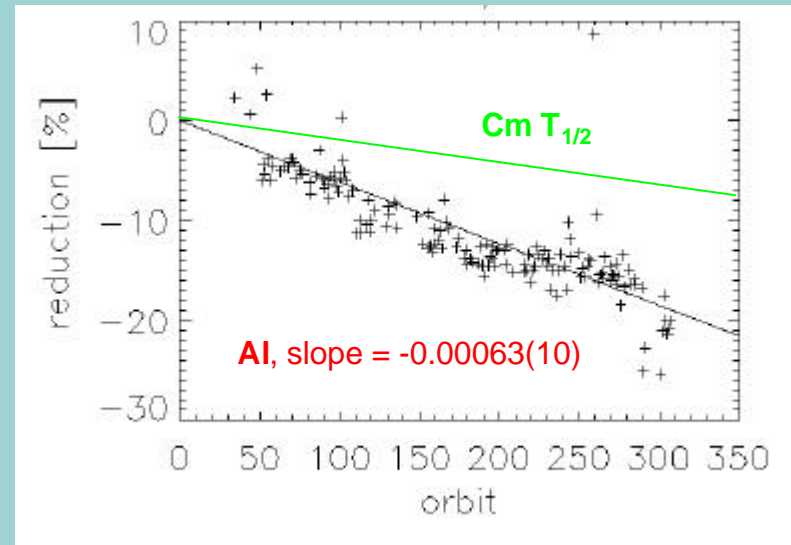
# In-orbit monitoring (2)

- Hot and flickering pixels (small fraction  $\ll 1\%$  with intensity which depends on time)
- Increase following solar events and gradual repair of defects (at  $-80^{\circ}\text{C}$ )



# In-orbit monitoring (3)

- Contamination verified using intensity of the onboard calibration sources
  - Al and F continuously illuminate parts of CCD
  - No significant difference in slope (but also not consistent with  $T_{1/2}$  of Cm source)
  - No contamination on detector
  - Marginal contamination on source stopping a particles



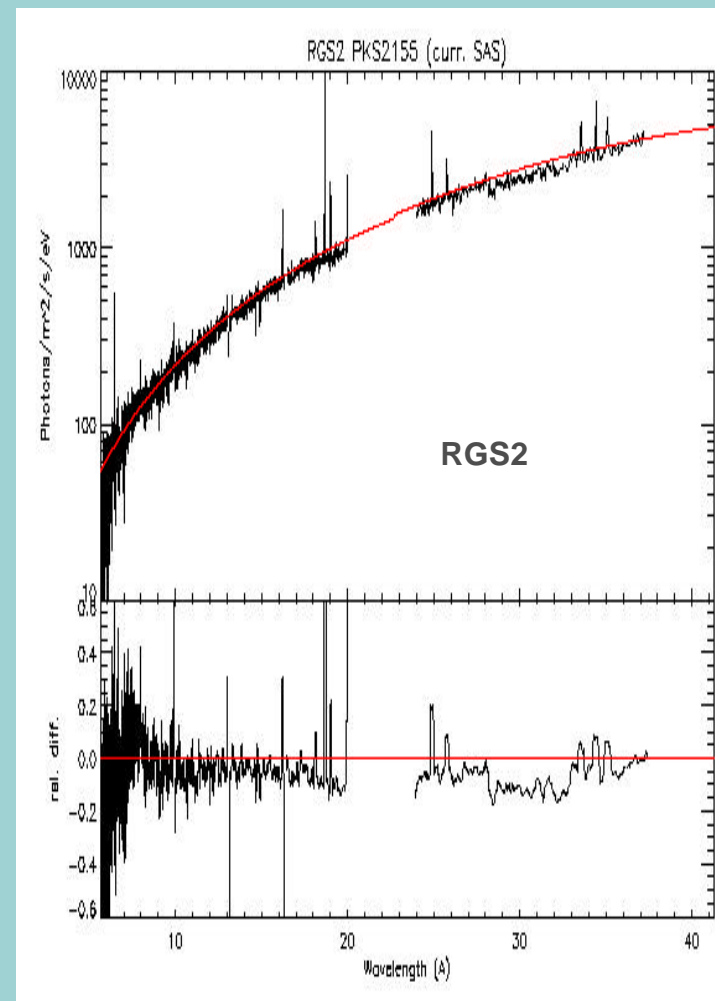
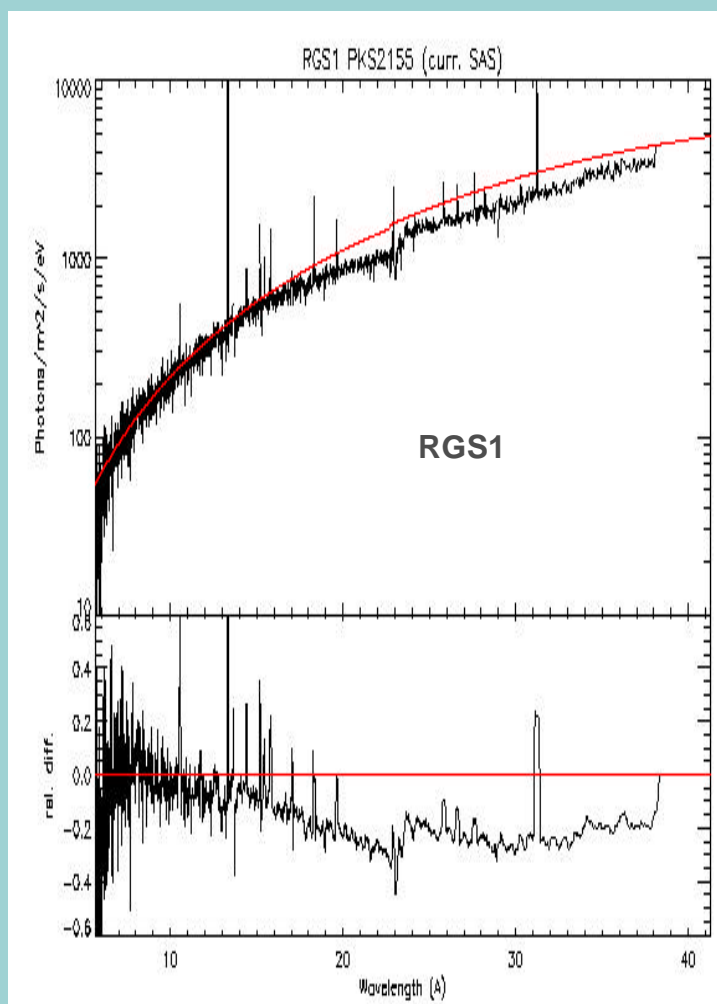
# SAS products

- SAS version 5.2 (and related CCFs) give reasonable results
- Not included are:
  - correction to force RGS1 to RGS2 ( $\beta$  dependent)
  - Correction for second orders
  - Proper vignetting function of the gratings
  - Proper description of O-edge including fine structure
- Without these corrections LSF,  $\lambda$  scale are correct,  $A_{\text{eff}}$  less accurate
- After these corrections response can be normalized to reference source



# SAS products (2)

- Not all parts of calibration in public version of SAS (yet)





# Conclusions

- Quality of calibrations in good agreement with pre-flight predictions based on a physical model of the instrument
- Improvements are feasible in 1 scale and response model (but require significant further work)
- Normalization of response to PKS2155 reduces uncertainties
- In-orbit performance as expected
- Current public SAS reasonable but various improvements identified to improve  $A_{\text{eff}}$

